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Joint Estimation of Carrier Frequency Offset and Channel Complex Gains for OFDM Systems in Fast Time-varying Vehicular Environments

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Abstract—In this paper, the physical nature of the radio-channel is considered by using an L -path channel model to develop an algorithm for OFDM systems operating in fast time-varying vehicular environment. Assuming the Time of Arrival (TOA) is known, a novel iterative pilot-aided algorithm for joint estimation of multi-path Rayleigh channel complex gains and Carrier Frequency Offset (CFO) is introduced. Each complex gain time-variation, within one OFDM symbol, is approximated by a Basis Expansion Model (BEM) representation. An autoregressive (AR) model is built for the parameters to be estimated (the AR model for the BEM coefficients is based on the Jakes process). The algorithm performs recursive estimation using Extended Kalman Filtering. Hence, the channel matrix is easily computed, and the data symbol is estimated with free inter-sub-carrier-interference (ICI) when the channel matrix is QR-decomposed. It is shown that only one iteration is sufficient to achieve the performance of the ideal case where knowledge of channel response and CFO is available.

I. INTRODUCTION

ORTHOGONAL frequency division multiplexing (OFDM) has become a standard technique for many wireless networks. However, it is well known that small carrier frequency offsets (CFOs) yield severe degradation in OFDM modulation since it produces inter-carrier interference (ICI) and attenuates the desired signal. These effects reduce the effective signal-to-noise ratio (SNR) in OFDM reception resulting in degraded system performance [1] [2]. CFOs are mainly caused by two different factors: Doppler effects and oscillator inaccuracies in the transmitter and receiver. Frequently, these two quantities are grouped together and modeled as a single frequency offset as in [3][4]. However, this model is not sufficiently accurate since separate offset parameter is needed for each propagation path given that the Doppler shift depends on the angle of arrival, which is peculiar to each path. Recently, it has been proposed to track directly the channel paths, which permits to take into account separate Doppler for each path [5][6]. Those works estimate the equivalent discrete-time channel taps ([6]) or the real path complex gains ([5]), which are both modeled by a basis expansion model (BEM). The BEM methods are Karhunen-Loeve BEM (KL-BEM), prolate spheroidal BEM (PS-BEM), complex exponential BEM (CE-BEM) and polynomial BEM (P-BEM).

However the CFO due to the mismatch between transmitter and receiver oscillators is not taken into account in those algorithms. In this paper, we propose a complete algorithm capable of estimating this CFO together with the time-variation of each channel path. To further improve the estimation accuracy, the algorithm uses decision feedback. Hence, the accuracy of the channel estimation, frequency offset estimation and symbol detection are enhanced simultaneously. Note also that since the pilots are used for both channel and frequency offset estimation, the pilot usage efficiency is greatly improved.

Generally, it is preferable to directly estimate the physical channel parameters [7] [5], instead of the equivalent discrete-time channel taps [6]. Indeed, as the channel delay spread increases, the number of channel taps also increases, thus leading to a large number of BEM coefficients, and consequently more pilot symbols are needed. Estimating the physical propagation parameters means estimating multi-path TOAs and multi-path complex gains. Note that the TOAs can be safely assumed invariant (at least during a block of several OFDM symbols). In this work, they are assumed perfectly estimated. It should be noted that an initial, and generally accurate estimation of the number of paths and TOAs can be obtained by using the MDL (minimum description length) and ESPRIT (estimation of signal parameters by rotational invariance techniques) methods [7][8].

Generally, the CFO due to the oscillator mismatch is considered constant during the transmission. One reason for this is that oscillators drift with temperature, supply voltage, load, and other slowly changing environmental parameters. However, depending on communication duration, time-varying CFO can be significant in a real physical environment. Our algorithm is able to track the CFO in case of variation. Our algorithm is a recursive algorithm based on Extended Kalman Filtering (EKF) combined with QR-equalization for data detection.

This paper is organized as follows: Section II introduces the OFDM system and the BEM modeling. Section III describes the AR model for the BEM coefficients and the Extended Kalman Filter. Section IV covers the algorithm for joint channel estimation and data recovery. Section V presents the simulations results which validate our technique. Finally, our conclusions are presented in Section VI.

The notations adopted are as follows: Upper (lower) bold face letters denote matrices (column vectors). $[\mathbf{x}]_k$ denotes the k th element of the vector $\mathbf{x}$, and $[\mathbf{X}]_{k,m}$ denotes the $[k, m]$ th element of the matrix $\mathbf{X}$ (note that the indices begin from 0). $\mathbf{I}_N$ is a $N \times N$ identity matrix and $\mathbf{0}_N$ is a $N \times N$ matrix of zeros. $\text{diag}\{\mathbf{x}\}$ is a diagonal matrix with $\mathbf{x}$ on its main diagonal and $\text{blkdiag}\{\mathbf{X}, \mathbf{Y}\}$ is a block diagonal matrix with the matrices $\mathbf{X}$ and $\mathbf{Y}$ on its main diagonal. The superscripts $(\cdot)^T$, $(\cdot)^*$ and $(\cdot)^H$ stand respectively for transpose, conjugate and Hermitian operators. $\mathbb{E}[\cdot]$ is the expectation operation. $J_0(\cdot)$ is the zeroth-order Bessel function of the first kind. $\nabla_{\mathbf{x}}$ represents the first-order partial derivative operator i.e., $\nabla_{\mathbf{x}} = [\frac{\partial}{\partial x_1}, \dots, \frac{\partial}{\partial x_N}]^T$.

II. SYSTEM MODEL

A. OFDM System Model

Consider an OFDM system with N sub-carriers, and a cyclic prefix length N_g . The duration of an OFDM block is $T = N_s T_s$, where T_s is the sampling time and $N_s = N + N_g$. Let $\mathbf{x}_n = [x_n[-\frac{N}{2}], x_n[-\frac{N}{2} + 1], \dots, x_n[\frac{N}{2} - 1]]^T$ be the n th transmitted OFDM symbol and $\{x_n[b]\}$ are normalized symbols (i.e., $\mathbb{E}[x_n[b]x_n^*[b]] = 1$). The frequency mismatch between the oscillators used in the radio transmitters and receivers causes a CFO ΔF . The normalized CFO is denoted $\nu = \Delta F N T_s$. After transmission over a multi-path Rayleigh channel, the n th received OFDM symbol $\mathbf{y}_n$, where $\mathbf{y}_n = [y_n[-\frac{N}{2}], y_n[-\frac{N}{2} + 1], \dots, y_n[\frac{N}{2} - 1]]^T$ is given by [9] [6]:

$$\mathbf{y}_n = \mathbf{H}_n \mathbf{x}_n + \mathbf{w}_n \quad (1)$$

where $\mathbf{w}_n = [w_n[-\frac{N}{2}], w_n[-\frac{N}{2} + 1], \dots, w_n[\frac{N}{2} - 1]]^T$ is a white complex Gaussian noise vector of covariance matrix $\sigma^2 \mathbf{I}_N$ and $\mathbf{H}_n$ is the $N \times N$ channel matrix. The elements of $\mathbf{H}_n$ can be written in terms of equivalent channel taps [10] $\{g_l^{(n)}(qT_s) = g_l(nT + qT_s)\}$:

$$[\mathbf{H}_n]_{k,m} = \frac{1}{N} \sum_{l=0}^{L'-1} \left[e^{-j2\pi(\frac{m}{N} - \frac{1}{2}) \cdot l} \sum_{q=0}^{N-1} e^{j2\pi \frac{\nu q}{N}} g_l^{(n)}(qT_s) e^{j2\pi \frac{m-k}{N} q} \right], \quad (2)$$

or in terms of physical channel parameters [8] (delays $\{\tau_l\}$ and complex gains $\{\alpha_l^{(n)}(qT_s) = \alpha_l(nT + qT_s)\}$), yielding:

$$[\mathbf{H}_n]_{k,m} = \frac{1}{N} \sum_{l=0}^{L'-1} \left[e^{-j2\pi(\frac{m}{N} - \frac{1}{2}) \tau_l} \sum_{q=0}^{N-1} e^{j2\pi \frac{\nu q}{N}} \alpha_l^{(n)}(qT_s) e^{j2\pi \frac{m-k}{N} q} \right]. \quad (3)$$

$L' < N_g$ and L are respectively the number of channel taps and the number of paths. The delays are normalized by T_s and not necessarily integers ($\tau_l < N_g$). The L elements of $\{\alpha_l^{(n)}(qT_s)\}$ are uncorrelated. However, the L' elements of $\{g_l^{(n)}(qT_s)\}$ are correlated, unless that the delays are multiple of T_s as mostly assumed in the literature. They are wide-sense

stationary (WSS), narrow-band zero-mean complex Gaussian processes of variances $\sigma_{g_l}^2$ and $\sigma_{\alpha_l}^2$, with the so-called Jakes' power spectrum of maximum Doppler frequency f_d [11]. The average energy of the channel approach is normalized to one, i.e., $\sum_{l=0}^{L'-1} \sigma_{g_l}^2 = 1$ and $\sum_{l=0}^{L-1} \sigma_{\alpha_l}^2 = 1$.

In the sequel, we will make the calculus based on the second approach (physical channel) and we can deduce the results of the first approach (channel taps) by replacing L by L' and the set of delays $\{\tau_l\}$ by $\{l, l = 0 : L' - 1\}$.

B. BEM Channel Model

Since the number of samples to be estimated LN_s is greater than the number of observation equations N , it is not efficient to estimate the time-variation of the complex gains, using directly the observation model in (1). Thus, we need to reduce the number of parameters to be estimated. In this section, our aim is to accurately model the time-variation of $\alpha_l^{(n)}(qT_s)$ by using a BEM. Collecting the samples of the l th path within the n th OFDM symbol in a $N_s \times 1$ vector $\boldsymbol{\alpha}_l^{(n)} = [\alpha_l^{(n)}(-N_g T_s), \dots, \alpha_l^{(n)}((N-1)T_s)]^T$, we can express $\boldsymbol{\alpha}_l^{(n)}$ as:

$$\boldsymbol{\alpha}_l^{(n)} = \boldsymbol{\alpha}_{\text{BEM}_l}^{(n)} + \boldsymbol{\xi}_l^{(n)} = \mathbf{Q} \mathbf{c}_l^{(n)} + \boldsymbol{\xi}_l^{(n)} \quad (4)$$

where $\mathbf{Q} = [\mathbf{q}_0, \dots, \mathbf{q}_{N_c-1}]$ is a $N_s \times N_c$ matrix that collects N_c orthonormal basis function $\mathbf{q}_d$ as columns, $\mathbf{c}_l^{(n)} = [c_{(0,l)}^{(n)}, \dots, c_{(N_c-1,l)}^{(n)}]^T$ represents the N_c BEM coefficients for the l th complex gain of the n th OFDM symbol, and $\boldsymbol{\xi}_l^{(n)}$ represents the corresponding BEM modeling error, which is assumed to be minimized in the MSE sense [12] [13]. Under this criterion, the optimal BEM coefficients and the corresponding model error are given by:

$$\mathbf{c}_l^{(n)} = (\mathbf{Q}^H \mathbf{Q})^{-1} \mathbf{Q}^H \boldsymbol{\alpha}_l^{(n)} \quad (5)$$

$$\boldsymbol{\xi}_l^{(n)} = (\mathbf{I}_{N_s} - \mathbf{S}) \boldsymbol{\alpha}_l^{(n)} \quad (6)$$

where $\mathbf{S} = \mathbf{Q} (\mathbf{Q}^H \mathbf{Q})^{-1} \mathbf{Q}^H$ is a $N_s \times N_s$ matrix. It provides the MMSE approximation for all BEM containing N_c coefficients, given by:

$$\text{MMSE}_l = \frac{1}{N_s} \mathbb{E} [\boldsymbol{\xi}_l^{(n)} \boldsymbol{\xi}_l^{(n)H}] \quad (7)$$

$$= \frac{1}{N_s} \text{Tr} \left((\mathbf{I}_{N_s} - \mathbf{S}) \mathbf{R}_{\boldsymbol{\alpha}_l^{(n)}}^{(0)} (\mathbf{I}_{N_s} - \mathbf{S}^H) \right) \quad (8)$$

where $\mathbf{R}_{\boldsymbol{\alpha}_l^{(n)}}^{(s)} = \mathbb{E} [\boldsymbol{\alpha}_l^{(n)} \boldsymbol{\alpha}_l^{(n-s)H}]$ is the $N_s \times N_s$ correlation matrix of $\boldsymbol{\alpha}_l^{(n)}$ with elements given by:

$$[\mathbf{R}_{\boldsymbol{\alpha}_l^{(n)}}^{(s)}]_{k,m} = \sigma_{\alpha_l}^2 J_0 \left(2\pi f_d T_s (k - m + s N_s) \right) \quad (9)$$

Various traditional BEM designs have been reported to model the channels time-variations, e.g., the CE-BEM $[\mathbf{Q}]_{k,m} = e^{j2\pi(\frac{k-N_g}{N_s})(m-\frac{N_c-1}{2})}$ [14], the GCE-BEM $[\mathbf{Q}]_{k,m} = e^{j2\pi(\frac{k-N_g}{N_s})(m-\frac{N_c-1}{2})}$ with $1 < a \leq \frac{N_c-1}{2f_d T}$ [12], the P-BEM $[\mathbf{Q}]_{k,m} = (k - N_g)^m$ [13] and the DKL-BEM which employs

basis sequences that corresponds to the most significant eigenvectors of the autocorrelation matrix $\mathbf{R}_{\alpha_l}^{(0)}$ [15]. From now on, we can describe the OFDM system model derived previously in terms of the BEM. Substituting (4) in (1) and neglecting the BEM model error, we obtain after some algebra:

$$\mathbf{y}_n = \mathcal{K}_n(\nu) \cdot \mathbf{c}_n + \mathbf{w}_n \quad (10)$$

where the $LN_c \times 1$ vector $\mathbf{c}_n$ and the $N \times LN_c$ matrix $\mathcal{K}_n$ are given by:

$$\mathbf{c}_n = \left[\mathbf{c}_0^{(n)T}, \dots, \mathbf{c}_{L-1}^{(n)T} \right]^T \quad (11)$$

$$\mathcal{K}_n(\nu) = \frac{1}{N} \left[\mathbf{Z}_0^{(n)}(\nu), \dots, \mathbf{Z}_{L-1}^{(n)}(\nu) \right] \quad (12)$$

$$\mathbf{Z}_l^{(n)}(\nu) = [\mathbf{M}_0(\nu) \text{diag}\{\mathbf{x}_n\} \mathbf{f}_l, \dots, \mathbf{M}_{N_c-1}(\nu) \text{diag}\{\mathbf{x}_n\} \mathbf{f}_l] \quad (13)$$

where vector $\mathbf{f}_l$ is the l th column of the $N \times L$ Fourier matrix $\mathbf{F}$ and $\mathbf{M}_d(\nu)$ is a $N \times N$ matrix given by:

$$[\mathbf{F}]_{k,l} = e^{-j2\pi(\frac{k}{N} - \frac{1}{2})\tau_l} \quad (14)$$

$$[\mathbf{M}_d(\nu)]_{k,m} = \sum_{q=0}^{N-1} e^{j2\pi\frac{\nu q}{N}} [\mathbf{Q}]_{q+N_g,d} e^{j2\pi\frac{m-k}{N}q} \quad (15)$$

Moreover, the channel matrix can be easily computed by using the BEM coefficients [9]:

$$\mathbf{H}_n = \sum_{d=0}^{N_c-1} \mathbf{M}_d(\nu) \text{diag}\{\mathbf{F}\chi_d^{(n)}\} \quad (16)$$

where $\chi_d^{(n)} = [c_{(d,0)}^{(n)}, \dots, c_{(d,L-1)}^{(n)}]^T$.

III. AR MODEL AND EXTENDED KALMAN FILTER

A. The AR Model for $\mathbf{c}_n$

The optimal BEM coefficients $\mathbf{c}_l^{(n)}$ are correlated complex Gaussian variables with zero-means and correlation matrix given by:

$$\begin{aligned} \mathbf{R}_{\mathbf{c}_l}^{(s)} &= \mathbb{E}[\mathbf{c}_l^{(n)} \mathbf{c}_l^{(n-s)H}] \\ &= \left(\mathbf{Q}^H \mathbf{Q} \right)^{-1} \mathbf{Q}^H \mathbf{R}_{\alpha_l}^{(s)} \mathbf{Q} \left(\mathbf{Q}^H \mathbf{Q} \right)^{-1} \end{aligned} \quad (17)$$

Hence, the dynamics of $\mathbf{c}_l^{(n)}$ can be well modeled by an autoregressive (AR) process [16] [17] [8]. A complex AR process of order p can be generated as:

$$\mathbf{c}_l^{(n)} = \sum_{i=1}^p \mathbf{A}^{(i)} \mathbf{c}_l^{(n-i)} + \mathbf{u}_l^{(n)} \quad (18)$$

where $\mathbf{A}^{(1)}, \dots, \mathbf{A}^{(p)}$ are $N_c \times N_c$ matrices and $\mathbf{u}_l^{(n)}$ is a $N_c \times 1$ complex Gaussian vector with covariance matrix $\mathbf{U}_l$. From [9], it is sufficient to choose $p = 1$ to correctly model the coefficients. The matrices $\mathbf{A}^{(1)} = \mathbf{A}$ and $\mathbf{U}_l$ are the AR model parameters obtained by solving the set of Yule-Walker equations defined as:

$$\mathbf{A} = \mathbf{R}_{\mathbf{c}_l}^{(1)} \left(\mathbf{R}_{\mathbf{c}_l}^{(0)} \right)^{-1} \quad (19)$$

$$\mathbf{U}_l = \mathbf{R}_{\mathbf{c}_l}^{(0)} + \mathbf{A} \mathbf{R}_{\mathbf{c}_l}^{(-1)} \quad (20)$$

Using (18), we obtain the AR model of order 1 for $\mathbf{c}_n$:

$$\mathbf{c}_n = \mathcal{A}_{\mathbf{c}} \cdot \mathbf{c}_{n-1} + \mathbf{u}_{\mathbf{c}n} \quad (21)$$

where $\mathcal{A}_{\mathbf{c}} = \text{blkdiag}\{\mathbf{A}, \dots, \mathbf{A}\}$ is a $LN_c \times LN_c$ matrix and $\mathbf{u}_{\mathbf{c}n} = [\mathbf{u}_0^{(n)T}, \dots, \mathbf{u}_{L-1}^{(n)T}]^T$ is a $LN_c \times 1$ zero-mean complex Gaussian vector with covariance matrix $\mathbf{U}_{\mathbf{c}} = \text{blkdiag}\{\mathbf{U}_0, \dots, \mathbf{U}_{L-1}\}$.

B. The AR Model for ν_n

Let us write the order 1 AR model for ν_n as follows:

$$\nu_n = a \cdot \nu_{n-1} + u_{\nu_n} \quad (22)$$

Since the CFO can be assumed as constant during the observation interval, a is considered to be close to 1, $a = 0.99$. The state noise parameter u_{ν_n} is assumed to be zero-mean complex Gaussian with variance σ_ν^2 .

C. State equation

Now, let us write the state-variable model. The state vector at time instance n consists of the BEM coefficients $\mathbf{c}_n$ and the vector of CFO ν_n :

$$\boldsymbol{\mu}_n = [\mathbf{c}_n^T, \nu_n^T]^T \quad (23)$$

There are LN_c BEM coefficients and 1 CFO values in the state vector of dimension $LN_c + 1 \times 1$. Then the linear state equation may be written as follows:

$$\boldsymbol{\mu}_n = \mathcal{A} \cdot \boldsymbol{\mu}_{n-1} + \mathbf{u}_n \quad (24)$$

where the state transition matrix is defined as follows:

$$\mathcal{A} = \text{blkdiag}\{\mathcal{A}_{\mathbf{c}}, a\} \quad (25)$$

The $LN_c + 1 \times 1$ noise vector is such that $\mathbf{u}_n = [\mathbf{u}_{\mathbf{c}n}^T, u_{\nu_n}]^T$ with covariance matrix $\mathbf{U} = \text{blkdiag}\{\mathbf{U}_{\mathbf{c}}, \sigma_\nu^2\}$.

D. Extended Kalman Filter (EKF)

The measurement equation (10) can be reformulated as:

$$\mathbf{y}_n = \mathbf{g}(\boldsymbol{\mu}_n) + \mathbf{w}_n \quad (26)$$

where the nonlinear function $\mathbf{g}$ of the state vector $\boldsymbol{\mu}_n$ is defined as $\mathbf{g}(\boldsymbol{\mu}_n) = \mathcal{K}_n(\nu) \cdot \mathbf{c}_n$. Nonlinearity of the measurement equation (26) is caused by CFO. The BEM coefficients are still linearly related to observations. Since the measurement equation is nonlinear, we use the Extended Kalman filter to adaptively track $\boldsymbol{\mu}_n$. Let $\hat{\boldsymbol{\mu}}_{(n|n-1)}$ be our a priori state estimate at step n given knowledge of the process prior to step n , $\hat{\boldsymbol{\mu}}_{(n|n)}$ be our a posteriori state estimate at step n given measurement $\mathbf{y}_n$ and, $\mathbf{P}_{(n|n-1)}$ and $\mathbf{P}_{(n|n)}$ are the a priori and the a posteriori error estimate covariance matrix of size $LN_c + 1 \times LN_c + 1$, respectively. We initialize the EKF with $\hat{\boldsymbol{\mu}}_{(0|0)} = \mathbf{0}_{LN_c+1,1}$ and $\mathbf{P}_{(0|0)}$ given by:

$$\mathbf{P}_{(0|0)} = \text{blkdiag}\{\mathbf{R}_{\mathbf{c}}^{(0)}, b\} \quad (27)$$

$$\mathbf{R}_{\mathbf{c}}^{(s)} = \text{blkdiag}\{\mathbf{R}_{\mathbf{c}_0}^{(s)}, \dots, \mathbf{R}_{\mathbf{c}_{L-1}}^{(s)}\}$$

where $\mathbf{R}_{\mathbf{c}_l}^{(s)}$ is the correlation matrix of $\mathbf{c}_l^{(n)}$ defined in (17). To derive the EKF equations, we need to compute the Jacobian matrix $\mathbf{G}_n$ of $\mathbf{g}(\boldsymbol{\mu}_n)$ with respect to $\boldsymbol{\mu}_n$ and evaluated at $\hat{\boldsymbol{\mu}}_{(n|n-1)}$:

$$\mathbf{G}_n = \nabla_{\boldsymbol{\mu}_n}^T \mathbf{g}(\boldsymbol{\mu}_n) \big|_{\boldsymbol{\mu}_n = \hat{\boldsymbol{\mu}}_{(n|n-1)}} = \left[\nabla_{\mathbf{c}_n}^T \mathbf{g}(\boldsymbol{\mu}_n) \big|_{\boldsymbol{\mu}_n = \hat{\boldsymbol{\mu}}_{(n|n-1)}}, \nabla_{\nu_n}^T \mathbf{g}(\boldsymbol{\mu}_n) \big|_{\boldsymbol{\mu}_n = \hat{\boldsymbol{\mu}}_{(n|n-1)}} \right] \quad (28)$$

After computation, we find:

$$\mathbf{G}_n = [\mathcal{K}_n(\hat{\nu}_{(n|n-1)}), \mathcal{K}'_n(\hat{\nu}_{(n|n-1)})\hat{\mathbf{c}}_{(n|n-1)}] \quad (29)$$

where

$$\mathcal{K}'_n(\nu) = \frac{1}{N} [\mathbf{Z}'_0^{(n)}(\nu), \dots, \mathbf{Z}'_{L-1}^{(n)}(\nu)] \quad (30)$$

$$\mathbf{Z}'_l^{(n)}(\nu) = [\mathbf{M}'_0(\nu) \text{diag}\{\mathbf{x}_n\} \mathbf{f}_l, \dots, \mathbf{M}'_{N_c-1}(\nu) \text{diag}\{\mathbf{x}_n\} \mathbf{f}_l] \quad (31)$$

The $N \times N$ matrix $\mathbf{M}'_d(\nu)$ is given by:

$$[\mathbf{M}'_d(\nu)]_{k,m} = \sum_{q=0}^{N-1} j2\pi \frac{q}{N} e^{j2\pi \frac{\nu q}{N}} [\mathbf{Q}]_{q+N_g, d} e^{j2\pi \frac{m-k}{N} q} \quad (32)$$

The EKF is a recursive algorithm composed of two stages: Time Update Equations and Measurement Update Equations. These two stages are defined as:

Time Update Equations:

$$\begin{aligned} \hat{\boldsymbol{\mu}}_{(n|n-1)} &= \mathcal{A}\hat{\boldsymbol{\mu}}_{(n-1|n-1)} \\ \mathbf{P}_{(n|n-1)} &= \mathcal{A}\mathbf{P}_{(n-1|n-1)}\mathcal{A}^H + \mathbf{U} \end{aligned} \quad (33)$$

Measurement Update Equations:

$$\begin{aligned} \mathbf{K}_n &= \mathbf{P}_{(n|n-1)} \mathbf{G}_n^H (\mathbf{G}_n \mathbf{P}_{(n|n-1)} \mathbf{G}_n^H + \sigma^2 \mathbf{I}_N)^{-1} \\ \hat{\boldsymbol{\mu}}_{(n|n)} &= \hat{\boldsymbol{\mu}}_{(n|n-1)} + \mathbf{K}_n (\mathbf{y}_n - \mathbf{g}(\hat{\boldsymbol{\mu}}_{(n|n-1)})) \\ \mathbf{P}_{(n|n)} &= \mathbf{P}_{(n|n-1)} - \mathbf{K}_n \mathbf{G}_n \mathbf{P}_{(n|n-1)} \end{aligned} \quad (34)$$

where $\mathbf{K}_n$ is the Kalman gain. The Time Update Equations are responsible for projecting forward (in time) the current state and error covariance estimates to obtain the a priori estimates for the next time step. The Measurement Update Equations are responsible for the feedback, *i.e.*, for incorporating a new measurement into the a priori estimate to obtain an improved a posteriori estimate. The Time Update Equations can also be thought of a predictor equations, while the Measurement Update Equations can be thought of a corrector equations.

IV. JOINT DATA DETECTION AND EKF

In the iterative algorithm for joint data detection, channel and CFO extended Kalman estimation, the N_p pilots subcarriers are eventually inserted into the N subcarriers at the positions $\mathcal{P} = \{p_r \mid p_r = (r-1)L_f + 1, r = 1, \dots, N_p\}$, where L_f is the distance between two adjacent pilots. We use the the QR-equalizer [8] [18] for the data detection. The QR-equalizer allows us to estimate the data symbol with free ICI by performing a so-called QR-decomposition. The algorithm proceeds as follows:

initialization:

- $\hat{\boldsymbol{\mu}}_{(0|0)} = \mathbf{0}_{LN_c + N_R N_T, 1}$
- compute $\mathbf{P}_{(0|0)}$ as (27)

$n \leftarrow n + 1$:

- execute the Time Update Equations of EKF (33)
- compute the channel matrix by substituting $\boldsymbol{\mu}_n$ with the prediction parameters $\hat{\boldsymbol{\mu}}_{(n|n-1)}$ in (16)
- recursion: $i \leftarrow 1$
 - remove the pilot ICI from the received data subcarriers
 - Detection of data symbols
 - execute the Measurement Update Equations of EKF (34)
 - compute the channel matrix using (16) with the updated parameters
 - $i \leftarrow i + 1$

where i represents the iteration number.

V. SIMULATION

In this section, the performance of our recursive algorithm is evaluated in terms of MSE for the channel and CFO estimation and BER for data detection. The normalized channel model is GSM Rayleigh model with $L = 6$ paths and maximum delay $\tau_{max} = 10T_s$ (see table I) [19][20][9]. A 4QAM-OFDM system with normalized symbols, $N = 128$ subcarriers, $N_g = \frac{N}{8}$ subcarriers, $N_p = 32$ pilots (*i.e.*, $L_f = 4$) and $\frac{1}{T_s} = 2MHz$ is used (note that $(SNR)dB = (\frac{E_b}{N_0})dB + 3dB$). These parameters are selected in order to be in concordance with the standard Wimax IEEE802.16e. The MSE and the BER are evaluated under a rapid time-varying channel such as $f_d T = 0.1$ corresponding to a vehicle speed $V_m = 600km/h$ for $f_c = 2.5GHz$. We choose a GCE-BEM [12] and $N_c = 3$ coefficients to model the path complex gain of the channel. Most advanced technologies have oscillator frequency tolerance less than 1 ppm (*i.e.* $\nu = 0.16$ in normalized units). For the simulation, we choose $\nu = 0.1$.

Fig. 1 shows the MSE as a function of SNR. The MSE is simulated for three iterations and is shown for the CFO on the one hand and for the multi-path complex gain on the other hand. For reference, the MSEs obtained in Data Aided (DA) mode have been plotted. As expected, the MSEs obtained in Data Aided mode are lower than the MSEs obtained with just the pilots, especially at low SNR where the detection errors are the most important. At high SNR, the MSEs tend to the MSEs in DA mode. It is also observed that after 20 dB, there is no improvement any more. This is due to the fact that beyond 20 dB, the matrix to be inversed to compute the Kalman Gain in Eq. (34) becomes badly scaled. This issue can be attenuated by adding some noise on the main diagonal of this matrix.

Fig. 2 gives the BER performance of our proposed iterative algorithm. For reference, we also plotted performance obtained with perfect knowledge of channel response and CFO. It is shown that after just one iteration, our joint estimator can achieve the same Bit Error Rate (BER) as that of an ideal reference receiver with perfect knowledge of channel response and carrier frequency offset. This shows that our proposed iterative joint channel and frequency offset estimator is effective. Again, it is observed a degradation in the performance after 20 dB. However, most of the typical modern systems operate with a SNR less than 20 dB.

Path number	Average Power (dB)	Delay (T_s)
0	-7.219	0
1	-4.219	0.4
2	-6.219	1
3	-10.219	3.2
4	-12.219	4.6
5	-14.219	10

TABLE I
RAYLEIGH CHANNEL PARAMETERS

Fig. 1. Mean Square Error (MSE) as a function of SNR for $f_d T = 0.1$

VI. CONCLUSION

A new iterative algorithm which jointly estimates multipath complex gain and CFO has been presented. The algorithm is based on a parametric channel model. Extended Kalman filtering is used for parameter estimation and the data recovery is carried out by means of a QR-equalizer. Simulation results show that by estimating and removing the ICI at each iteration, the BER is greatly improved, especially after the first iteration. For a SNR < 20 dB (typical modern systems), our algorithm needs only one iteration to achieve the same performance than the ideal case where knowledge of the channel response and CFO is available. However, for a SNR > 20 dB, performance is degraded compared to the ideal case.

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Fig. 2. Bit Error Rate (BER) as a function of SNR for $f_d T = 0.1$

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